Abstract

In this paper, we introduce a practical modeling approach to improve the quality of polygonal mesh structures. Our approach is based on a discrete version of Gaussian-Bonnet theorem on piecewise planar manifold meshes and vertex angle deflections that determines local geometric behavior. Based on discrete Gaussian-Bonnet theorem, summation of angle deflections of all vertices is independent of mesh structure and it depends on only the topology of the mesh surface. Based on this result, it can be possible to improve organization of mesh structure of a shape according to its intended geometric structure.

1 Motivation

Most professional modelers in animation and special effect industry slowly migrated subdivision surfaces. One of the crucial questions for practical modeling with subdivision surfaces is to identify the numbers and types of extraordinary vertices that needs to be used for a successful modeling. In the first observation, this question seems easy to answer based on genus of the goal surface. Using Euler’s formula, we can compute the number of extraordinary vertices and their valences (also the number of faces and their valences) for the given genus.

However, extraordinary vertices do not result only from genus. In most practical cases, we need to consider the geometrical structure of the surface. Tree structures are especially the ones that cause problems. Tree structures are more common than real trees. For instance, the modelers introduce extraordinary vertices and their valences (also the number of faces and their valences) for the given genus.

By relating topology and geometry, we give a framework to answer such problems coming from practical modeling. Our results justify some of the intuitively developed practices in current modeling approaches. For instance, the modelers introduce extraordinary vertices to model eyes, nose and mouth in facial modeling. Our results go further than and even defies common sense about subdivision modeling. We show that despite the common belief the quality of some surfaces can be improved by introducing extraordinary vertices.

2 Introduction

Our approach is based on the Gauss-Bonnet Theorem that says that the integral of the Gaussian curvature over a closed smooth surface is equal to $2\pi \times$ the Euler characteristic of the surface which is $2 - 2g$ [Weisstein 2005]. The theorem requires a smooth surface. In this section, we provide a simple proof for Gauss-Bonnet Theorem on Piecewise Linear Meshes.

2.1 Piecewise Linear Meshes

We say that a mesh $M$ is piecewise linear if every edge of $M$ is a straight line segment, and every face of $M$ is planar. Piecewise linear meshes are useful since the surface of each face is well-defined [Williams 1972]. Most common piecewise linear meshes are triangular meshes. However, piecewise linear meshes are a significant generalization of triangular meshes, which not only allow non-triangular faces, but also allow faces to have different face valence. In the discussion of the current paper, we will be focused on piecewise linear meshes.

We start by some intuitions. Let $M$ be a piecewise linear mesh such that all vertices of $M$ have the same vertex valence $m$ and all faces of $M$ have the same face valence $n$ (such a mesh is called a regular mesh). Suppose that $M$ has $v$ vertices, $e$ edges, and $f$ faces. By Euler Equation [Hoffmann 1989; Mantyla 1988],

$$v - e + f = 2 - 2g$$

where $g$ is the genus of the mesh $M$ and from the equalities $m v = m f = 2e$, we derive

$$e = \frac{nm(2 - 2g)}{2n + 2m - nm}, \quad v = \frac{2m(2 - 2g)}{2n + 2m - nm}, \quad f = \frac{2m(2 - 2g)}{2n + 2m - nm}$$

We would like to generalize the above relations to piecewise linear meshes that are not regular. For this, we introduce the following definitions.

**Definition** Let $M$ be a piecewise linear mesh, with vertex set $\{\mu_1, \ldots, \mu_v\}$ and face set $\{\phi_1, \ldots, \phi_f\}$. Moreover, for each $i, 1 \leq i \leq v$, let $m_i$ be the valence of the vertex $\mu_i$, and for each $j, 1 \leq j \leq f$, let $n_j$ be the valence of the face $\phi_j$. Then the average vertex valence $m$ and the average face valence $n$ are defined, respectively, to be

$$m = \frac{\sum_{i=1}^{v} m_i}{v} \quad \text{and} \quad n = \frac{\sum_{j=1}^{f} n_j}{f}$$

Note that $m$ and $n$ are not necessarily integers.

Based on these new concepts, the number $v$ of vertices, the number $e$ of edges, and the number $f$ of faces in a piecewise linear mesh can be given as functions in terms of the average vertex valence, the average face valence, and the genus of the mesh, as shown in the following lemma.
Lemma 2.1 Let $M$ be a piecewise linear mesh. Suppose that $M$ has $v$ vertices, $e$ edges, $f$ faces, and genus $g$. Let $m$ and $n$ be the average vertex valence and average face valence, respectively, of the mesh $M$, then

\[
e = \frac{nm(2-2g)}{2n+2m-nm}, \quad v = \frac{2n(2-2g)}{2n+2m-nm}, \quad f = \frac{2m(2-2g)}{2n+2m-nm}
\]

Proof. Suppose that the vertex set of $M$ is \{$\mu_i$\} and that the face set of $M$ is \{$\phi_j$\}. Moreover, suppose that for each $i$, $1 \leq i \leq v$, the vertex $\mu_i$ has valence $m_i$, and that for each $j$, $1 \leq j \leq f$, the face $\phi_j$ has valence $n_j$. Since each edge in the mesh $M$ is used exactly twice in vertex valences and is used exactly twice in face valences, we have

\[
\sum_{i=1}^{v} m_i = \sum_{j=1}^{f} n_j = 2e
\]

On the other hand, by our definitions of the average vertex valence $m$ and the average face valence $n$, we have

\[
mv = \sum_{i=1}^{v} m_i \quad \text{and} \quad nf = \sum_{j=1}^{f} n_j
\]

Therefore, we still have $mv = nf = 2e$. Since the mesh $M$ has genus $g$, Equation (1) holds. Combining Equation (1) and the equalities $mv = nf = 2e$, we get immediately

\[
e = \frac{nm(2-2g)}{2n+2m-nm}, \quad v = \frac{2n(2-2g)}{2n+2m-nm}, \quad f = \frac{2m(2-2g)}{2n+2m-nm}
\]

This proves the lemma.

\[\square\]

2.2 Angle deflection at a vertex

To understand the local behavior around a vertex of a piecewise linear meshes, angle deflection are great tools. Angle deflection at a vertex are formally defined based on the corner angles around a vertex, as follows.

Definition Let $\mu_i$ be a vertex on a piecewise linear mesh $M$. The angle deflection at vertex $\mu_i$ is defined as

\[\bar{\theta}(\mu_i) = 2\pi - \sum_{j=1}^{m_i} \theta_j\]

where $\theta_j$ is the internal angle of the $j$-th corner of vertex $\mu_i$ and $m_i$ is the valence of the vertex $\mu_i$.

The importance of angle deflections to describe local behavior can be best understood by viewing developable sculptures [Koman 2005] of sculptor Ilhan Koman. He created a set of sculptures by forcing the total angle in a given point larger than $2\pi$ [Koman 2005]. As shown in Figure 1, when the angle goes beyond $2\pi$, it is possible to create a wide variety of saddle shapes. We observe that Koman’s developable structures can give very useful information about the local behavior at a vertex for piecewise linear meshes.

It is interesting to point out that the value of $\bar{\theta}(\mu_i)$ is somewhat related to curvature and based on the values of corner angles around the vertex $\mu_i$. More precisely,

- $\bar{\theta}(\mu_i) > 0$: then vertex $\mu_i$ is either convex or concave.

This is not unexpected since the most popular discrete version of Gaussian curvature introduced by Calladine for triangular meshes uses angular deflection [Calladine 1983]. Calladine’s discrete
Definition Let $M$ be a piecewise linear mesh with a vertex set $\{\mu_1, \ldots, \mu_v\}$. The sum of angle deflections (SAD) of the mesh $M$ is defined as

$$\bar{\theta}(M) = \sum_{i=1}^{v} \bar{\theta}(\mu_i)$$

Note that the SAD of a piecewise linear mesh is closely related to the geometric shape of the mesh $M$. On the other hand, as we will prove in the following theorem, the SAD of a mesh is a topological invariant.

**Theorem 2.2** Let $M$ be a piecewise linear mesh of genus $g$. Then the SAD $\bar{\theta}(M)$ of the mesh $M$ is equal to $2\pi(2-2g)$.

**Proof.** Let $\{\mu_1, \ldots, \mu_v\}$, $\{e_1, \ldots, e_e\}$, and $\{\phi_1, \ldots, \phi_f\}$ be the vertex set, edge set, and face set of the mesh $M$, respectively. Moreover, for each $i$, $1 \leq i \leq v$, let $n_i$ be the valence of the vertex $\mu_i$, and for each $j$, $1 \leq j \leq f$, let $n_j$ be the valence of the face $\phi_j$. Let $m$ and $n$ be the average vertex valence and the average face valence, respectively, of the mesh $M$.

Consider each face $\phi_j$ of valence $n_j$. Since $\phi_j$ is a planar polygon, the sum $\sigma(\phi_j)$ of inner angles of $\phi_j$ is equal to $(n_j - 2)\pi$. Adding this up over all faces in the mesh $M$, we obtain

$$\sum_{j=1}^{f} \sigma(\phi_j) = \sum_{j=1}^{f} (n_j - 2)\pi = \left(\sum_{j=1}^{f} n_j - 2f\right)\pi = nf\pi - 2f\pi \quad (2)$$

where we have used the definition of the average face valence $n = (\sum_{j=1}^{f} n_j)/f$.

On the other hand, by the definition of angle deflections, the sum of corner angles around each vertex $\mu_i$ of the mesh $M$ is equal to $2\pi - \bar{\theta}(\mu_i)$. Adding this up over all vertices in the mesh $M$, we get

$$\sum_{i=1}^{v} (2\pi - \bar{\theta}(\mu_i)) = 2v\pi - \bar{\theta}(M)$$

This value should be equal to the value in (2) since both of them are the sum of the total corner angles in the mesh $M$. Therefore, we get

$$\bar{\theta}(M) = 2v\pi - nf\pi + 2f\pi = 2\pi(v - nf/2 + f)$$

By the definition of the average face valence $n = (\sum_{j=1}^{f} n_j)/f$, and noticing that $2\pi = \sum_{j=1}^{f} n_j$, we get immediately $nf/2 = \pi$. This gives

$$\bar{\theta}(M) = 2\pi(v - \pi + f)$$

By Euler Equation (1), we get

$$\bar{\theta}(M) = 2\pi(2-2g)$$

This proves the theorem.

Figure 3: The total adds up to $(2 - 2g)$ if we assign minima/maxima points +1 and saddles −1.

Figure 3 also give a visual explanation of the sum of angle deflections. In figure, we assume that all angle deflections occur only at critical points. If that were really the case, the angle deflection in each critical point would have been $+2\pi$ for minima/maxima and $-2\pi$ for each saddle point. So, the total will be equal to $2\pi(2-2g)$, which is the sum of angle deflections.

It is also clear from Figure 3 why branches do not change the total angle deflections. Each branch induces the same numbers of saddle points and maxima/minima points; so total effect becomes zero. On the other hand, each handle (i.e., each hole) introduces two saddle type critical points, which decreases the total angle deflections by $4\pi$.

3 Homogenous Operations

For branch creations, professional modelers usually use extrusion [Landreneau et al. 2005] and wrinkle operations (see Section 4). These operations are homogenous, i.e. they do not change mesh topology. Subdivision schemes, which are commonly used to create smooth surfaces, are also homogenous operations.
To understand why homogenous operations do not change the total angle deflections, it is insightful to look at them from a mesh topological point of view.

Let us assume that the number of faces, edges and vertices of a mesh increase in each application of homogenous operations. Based on this assumption, let us consider the practice in which when homogenous operations are applied to a mesh while the genus of the mesh stays the same, the numbers of faces, edges and vertices of the mesh increase without a limit.

**Remark 1.** This is not an unrealistic assumption. In fact, all subdivision schemes, extrusions and wrinkle operations increase the number of faces, edges and vertices.

To analyze repeated applications of homogenous operations we can again use the Euler equation. Let us consider specifically meshes of genus $g$. Let $n$ and $m$ be the average face valence and the average vertex valence of a mesh of genus 1. Using Euler equation (1) and equations in Lemma 2.1, we have

\[
\frac{2 - 2g}{e} = \frac{2}{m} + \frac{2}{n} - 1
\]

By our assumption $e$ can be arbitrarily large but the mesh genus stays the same, thus

\[
\frac{2}{m} + \frac{2}{n} - 1 \approx 0
\]

which gives

\[
m \approx \frac{2n}{n - 2}
\]

Under the assumption that $m \geq 3$ and $n \geq 3$, and replacing the above approximation by an equality, we will get

\[3 \leq n \leq 6\]

This result says that the average face valence cannot exceed 6 regardless of what we do (if we do not allow valent-2 vertices and polygons with two sides).

In other words, if our homogenous operations create only quadrilateral faces (i.e., $n = 4$), then the average vertex valence $m$ goes to 4. If the homogenous operations create only triangles (i.e., $n = 3$), then the average vertex valence $m$ goes to 6. For pentagons (i.e., $n = 5$), the average vertex valence approaches to $10/3$ and for hexagons (i.e., $n = 6$) it goes to 3. Any mixed use of different face types will create a rational number for the average vertex valence.

This also explains why most subdivision schemes provide (3, 6) [Kobbelt 2000; Loop 1987], (4, 4) [Doo and Sabin 1978; Catmull and Clark 1978; Peters and Reif 1997; Sabin 2000] and (6, 3) [Claes et al. 2002: Oswald and Schröder 2003; Akleman and Srinivasan November 2002] regular regions in which integer tuple $(n,m)$ satisfy the equation $\frac{2}{n} + \frac{2}{m - 1} = 0$. Note that in these subdivisions the number of regular vertices and faces (i.e vertices with valence $m$ and faces with valence $n$) increases, while the number of extraordi- nary vertices and faces stays the same in each iteration. As a result, the regular regions dominate the mesh.

**Remark 2.** To guarantee that subdivided mesh is at least $G^1$ continuous each face of subdivided mesh must approach a convex planar surface. So, we can say that most subdivision surfaces consist of piecewise linear approximations of curved faces. Piecewise linear approximations usually are (3, 6), (4, 4) or (6, 3) regular regions for most subdivision schemes [Akleman et al. 2004].

### 4 Implications on Practical Modeling with Homogenous Operations

Our results are particularly insightful for modeling better mesh structures for surfaces that include branches. We do not create branches only for modeling trees. Branches are important for modeling and they are everywhere. Even a simple genus-0 human face model must include branches such as eye sockets, nose and mouth.

**Remark 3** With better mesh structures, we mean faces are convex and as regular as possible. It is not always possible to make faces regular. For instance, we cannot get an angle deflection larger than $\pi$ with regular convex faces. However, it is still possible to make faces as regular as possible by using appropriate valence. For instance, if we force the regular mesh structures such as (4, 4), we cannot avoid irregular faces.

By introducing saddle and minima/maxima type of critical points we can obtain better mesh structure. In practice, that is what professional modelers do very efficiently. Based on our results, it is easy to introduce saddles and minima/maxima. If we use the same type of faces, assuming that all the faces are almost regular, all we have to do is to carefully control the valences of vertices. For instance, if we work only with triangles, we have to choose 3, 4 and 5 valent vertices in places we want to obtain minima or maxima. For saddle points, we have to choose valences of vertices larger than 6. Based on how complicated we want to design a saddle point, we can increase the valence.

Changing the valence can even improve the mesh structure of genus-1 surfaces. The Figure 4 shows an example of mesh improvement by decreasing and increasing valence in appropriate regions.

![Figure 4: This example shows that introducing non-regular structures can improve the mesh structure even for a simple genus-1 surface. See the thin quadrilaterals exists in regular (4, 4) structure on the left model. By increasing the valence of some vertices in saddle region and decreasing the valence of some vertices in convex region, release the tension and quadrilaterals look more regular.](image)
For professional modeling quadrilateral modeling is a particularly important. In quadrilateral modeling, for minima and maxima, we have only one choice, 3 valence vertices. For saddles we can use any valence higher than 4. Extrusions and wrinkle operations as shown in Figures 5 and 6 introduce minima/maxima and saddle points simultaneously and therefore, they are commonly by professional modelers used to create branches.

Figure 5: Branch creation with extrusion operation. Before extrusion we have a quadrilateral with 4-valent vertices. After extrusion 4 vertices have 5 valence and another 4 vertices have 3 valence. Average vertex valence added is 4.

Figure 6: Branch creation with wrinkle operation. After wrinkle operation, 4 vertices have 4 valence, 2 vertices have valence 3 and another 2 vertices have 5 valence. So, added average vertex valence is 4. Subdivided version shows how an eye or wrinkle is automatically created with this operation.

5 Conclusions and Future Work

In this paper, we have introduced an approach to improve mesh structures to use in practical modeling with homogenous operations. We show that vertex angle deflection can give a powerful insight about local geometric behavior to professional modelers. Based on a discrete version of Gauss-Bonnet theorem, we have shown that it is be possible to improve the organization of mesh structures of shapes according to their geometric structure.

Based on the results in this paper, it is possible to automatically create a better mesh from a given mesh. We think that vertex angle deflections can also be used to smooth the surfaces.

Despite the similarity, angle deflections are different than Gaussian curvature and its discrete versions. For instance, unlike sum of angle deflections, sum of discrete Gaussian Curvature may not be equal to $2\pi(2-2g)$. Both Gaussian curvature and angle deflections are rotation and translation invariant. However, Angle deflection is also scale invariant which can make it useful for shape retrieval.

An unexpected result coming from vertex angle deflection is paper folding. Since we know that the total angle will always stay constant, we can shape papers simply using staples\(^1\). Using this insight, we were able to shape papers intuitively. And we were able to create a variety of paper sculptures. Figure 7 shows two examples of paper sculptures we have created based on the insight coming from our result.

References


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\(^1\)Since papers are developable surfaces, we can think that papers are piecewise linear meshes that consist of thin stripes of planes. So our theorem applies to papers.
Figure 7: Paper sculptures. Cat mask is created from a 8.5 × 11 paper that is cut into one square and one rectangular pieces. These pieces are later stapled together to create the cat mask. Swan is created from a shaped and folded paper using only three staples.


